

SIEMENS

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Information
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Networks

Adaptive Compensation of Single Channel Distortions with Optical FIR-Filters at 40Gb/s

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Overview

- Adaptive Optical Distortion Compensation
 - Introduction
 - Concept of an Adaptive Optical Equalizer
 - FIR-Filter Structure
 - Simulation Results: Group Velocity Dispersion, Self-Phase Modulation, Polarization Mode Dispersion, Group Delay Ripple
 - Summary



Why Adaptive Distortion Compensation?

- Reconfigurable optical networks need adaptive equalization to follow the dynamic changes of the transmission channel:
 - chromatic dispersion
 - ◆ different routes through the network
 - ◆ temperature variations
 - nonlinear effects
 - ◆ signal distortions dependent on dispersion and signal power
 - PMD
 - ◆ birefringence and mode coupling variations

Enabling Technology ≥ 10 Gb/s



Adaptive Distortion Compensation

- existing concepts
 - electrical equalization by intersymbol interference minimization with Finite Impulse Response (FIR)-Filters, Decision Feedback Equalizer (DFE), Viterbi Equalizer

problem: envelope demodulation in the photo diode (PD)
 - optical compensation by inverse system modeling with e.g. DCF, CFBG, cascaded Mach-Zehnder Interferometers (MZI), Ring Resonators (RR), Etalons, VIPA

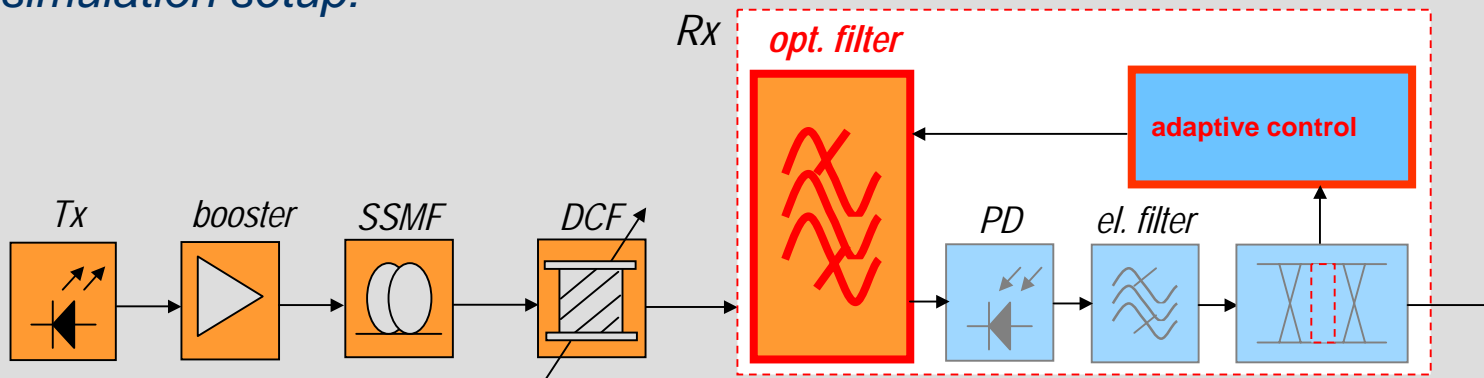
but: compensation of only a single fiber impairment

Adaptive Distortion Compensation

⇒ adaptive equalizer in the optical domain

- ◆ equalization before the PD, phase information available
- ◆ variable complex tap weights (el. filter: only real tap weights)
- ◆ maximization of the electrical eye opening by controlling the tap weights of the optical filter with an adaptive algorithm

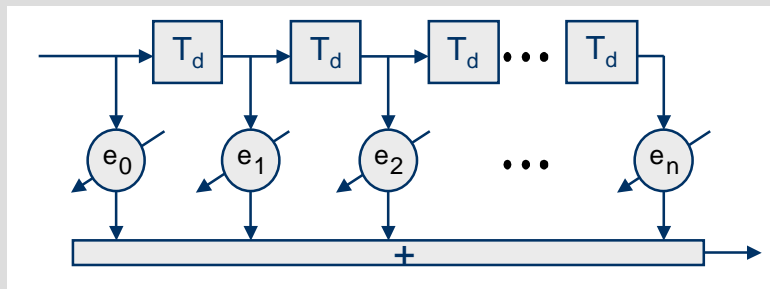
simulation setup:



combined optical equalization of
single channel distortions

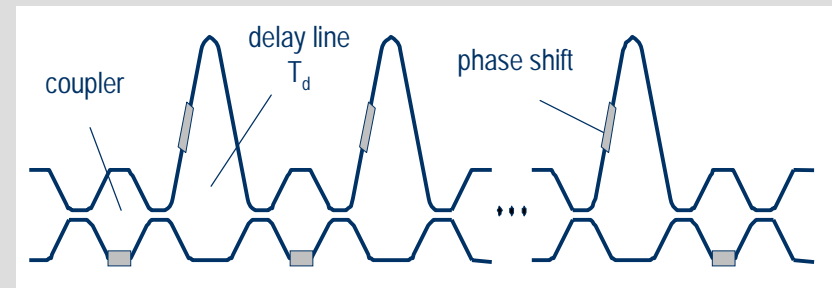
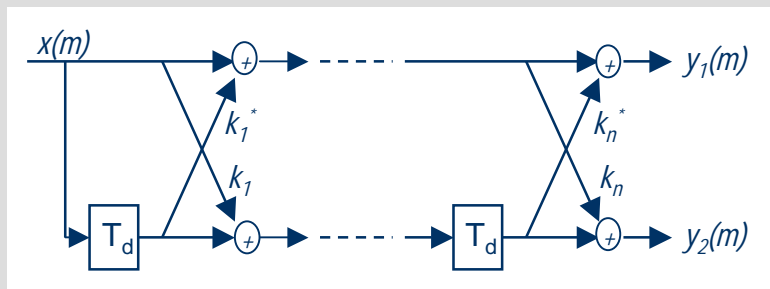
FIR - Filter Structure

- transversal structure



difficult to realize as optical filter
with variable complex tap
coefficients

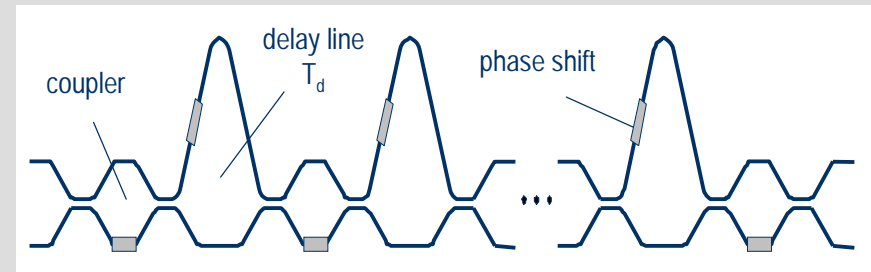
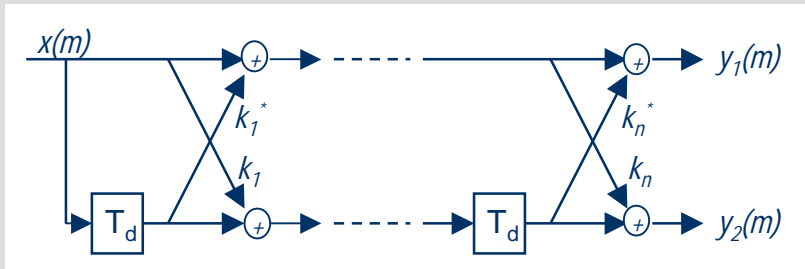
- lattice structure



cascaded Mach-Zehnder Interferometers

FIR - Filter Structure

lattice structure



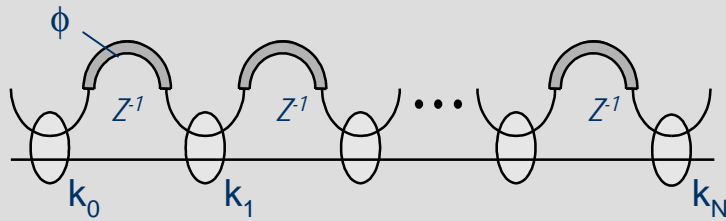
cascaded Mach-Zehnder Interferometers

- complex tap weights by changing the coupling and phase ratio
- the frequency response is periodic: $FSR=1/T_d$
 ⇒ *combined equalization of several channels*



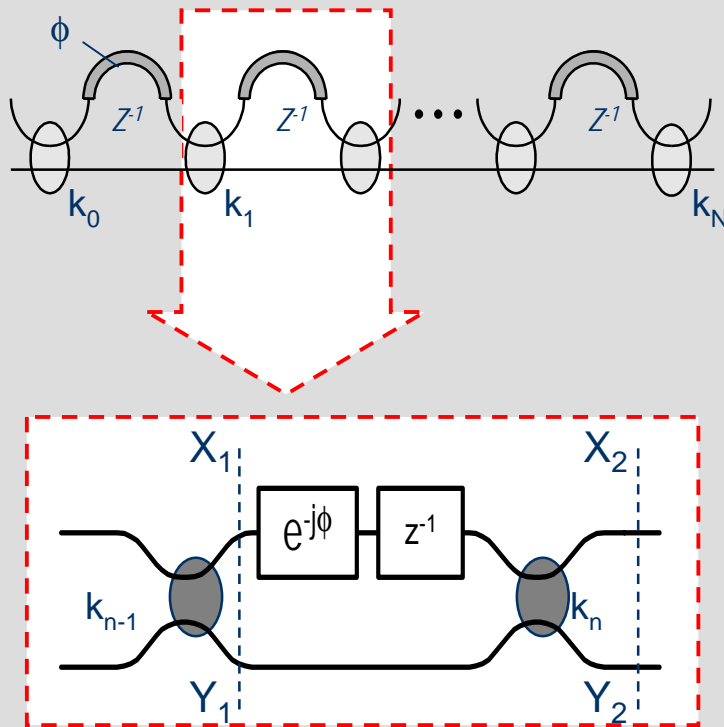
FIR - Filter Structure

- lattice structure



FIR - Filter Structure

- lattice structure



$$\begin{bmatrix} X_n(z) \\ Y_n(z) \end{bmatrix} = \Phi_n(z) \begin{bmatrix} X_{n-1}(z) \\ Y_{n-1}(z) \end{bmatrix}$$

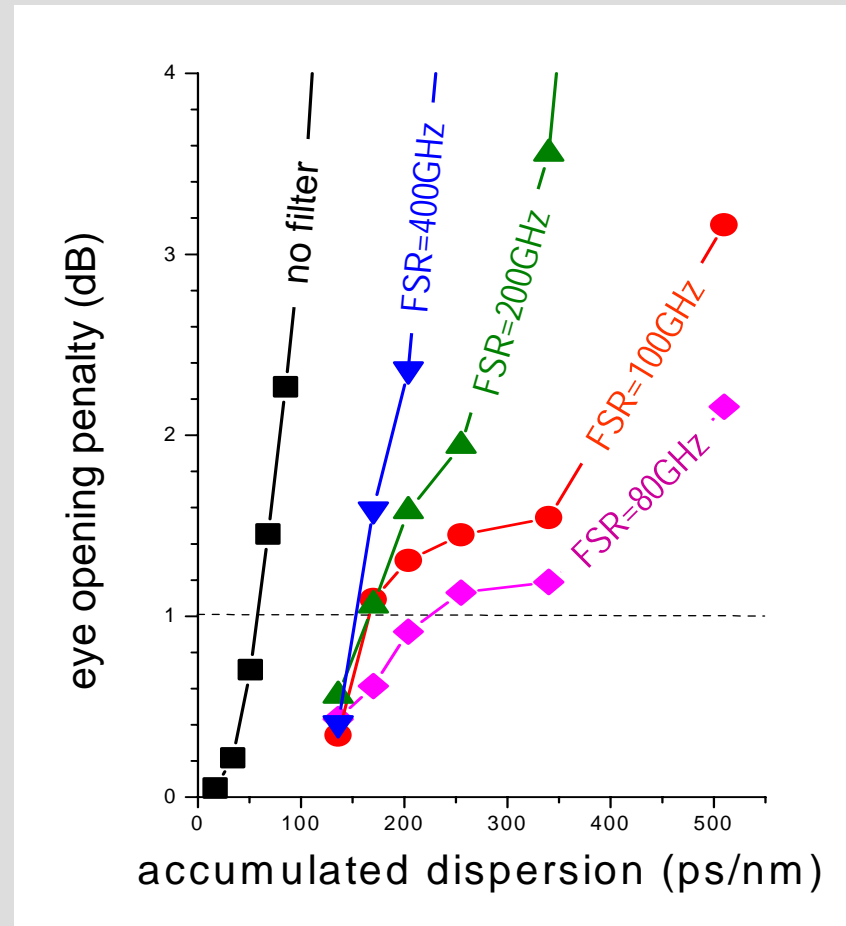
$$\begin{aligned} \Phi_n(z) &= \begin{bmatrix} c_n & -js_n \\ -js_n & c_n \end{bmatrix} \cdot \begin{bmatrix} z^{-1}e^{-j\phi_n} & 0 \\ 0 & 1 \end{bmatrix} \\ &= \begin{bmatrix} c_n z^{-1}e^{-j\phi_n} & -js_n \\ -js_n z^{-1}e^{-j\phi_n} & c_n \end{bmatrix} \end{aligned}$$

mit $c_n = \sqrt{1 - k_n}$, $s_n = \sqrt{k_n}$,

$$\begin{bmatrix} X_n(z) \\ Y_n(z) \end{bmatrix} = \Phi_N \cdots \Phi_1 \Phi_0 \begin{bmatrix} X_{in}(z) \\ Y_{in}(z) \end{bmatrix}$$

40Gb/s Results - GVD

- dispersion tolerance (1dB reference)
 - w/o equalizer: $D = \pm 60 \text{ ps/nm}$
 - ⇒ with equalizer: $D = \pm 200 \text{ ps/nm}$
- arbitrary accurate equalization with increasing filter order
- equalizing performance = $f(\text{FSR})$
 - increasing distortion ⇒ increasing pulse broadening
 - increasing FSR ⇒ decreasing T_d ⇒ shorter impulse response
 - increasing pulse broadening & shorter impulse response ⇒ decreasing equalization

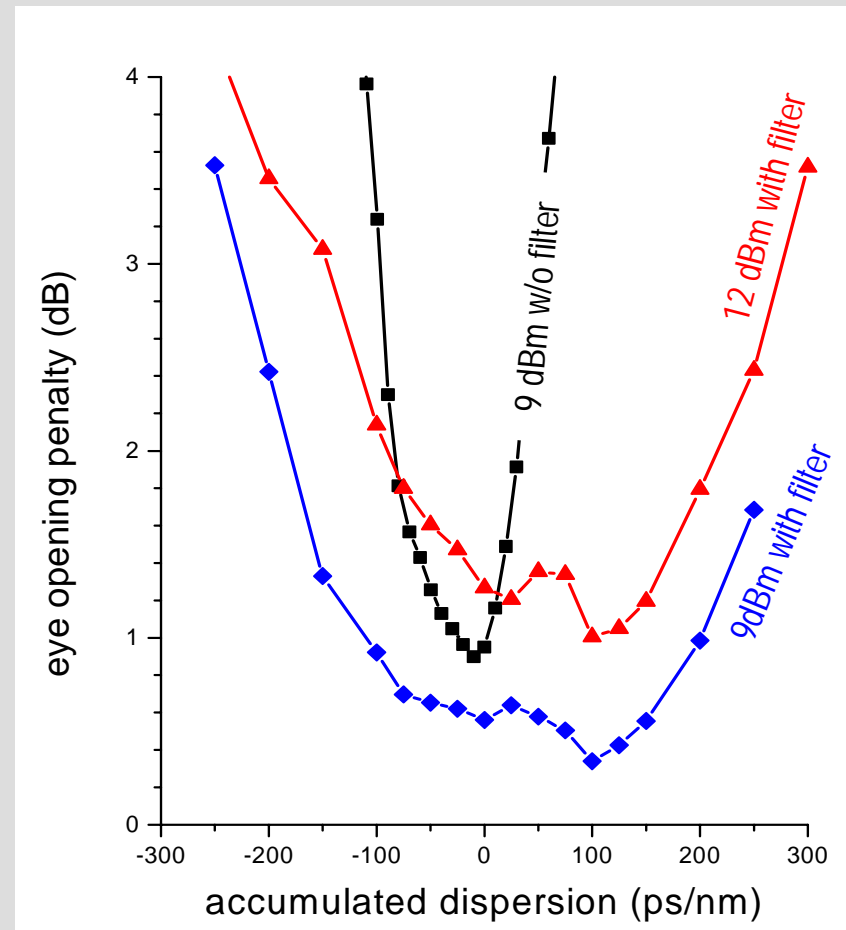


40 Gb/s, linear transmission, filter order: $n=10$

40Gb/s Results - SPM

- dispersion tolerance @ 9dBm
 - w/o equalizer: $D=0\text{ps/nm}$
 - ⇒ with equalizer: $D = -100 \dots +200 \text{ps/nm}$

 - SPM equalization (1dB reference)
 - w/o equalizer: $P_{\text{launch}} = 9 \text{ dBm}$
 - with equalizer: $P_{\text{launch}} = 12 \text{ dBm}$
- ⇒ *SPM equalizing gain: 3 dB*



40 Gb/s, nonlinear transmission, filter order: $n=10$



PMD Equalization Schemes

■ Adaptive Equalization:

- equalization with a single filter:

both orthogonal modes will be equalized with the same transfer function

⇒ *slight improvement, eye cosmetics*

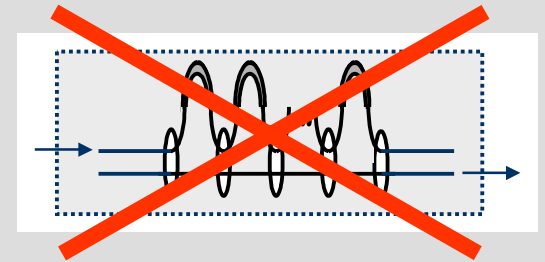
- equalization with 2 transfer functions:

by including a polarization beam splitter (PBS) both orthogonal modes see a different transfer function

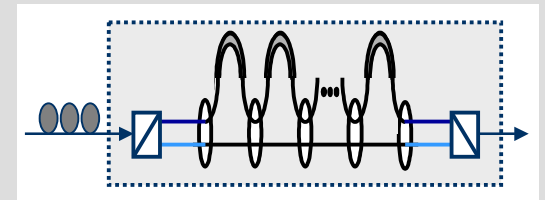
⇒ *excellent improvement*

⇒ *max $DGD_{komp} = n \cdot T_d$*

1.)

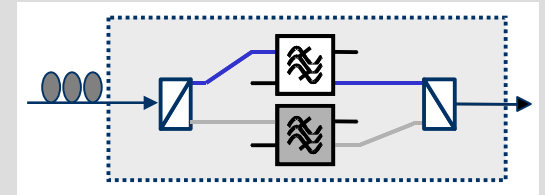


2a.)



single filter setup

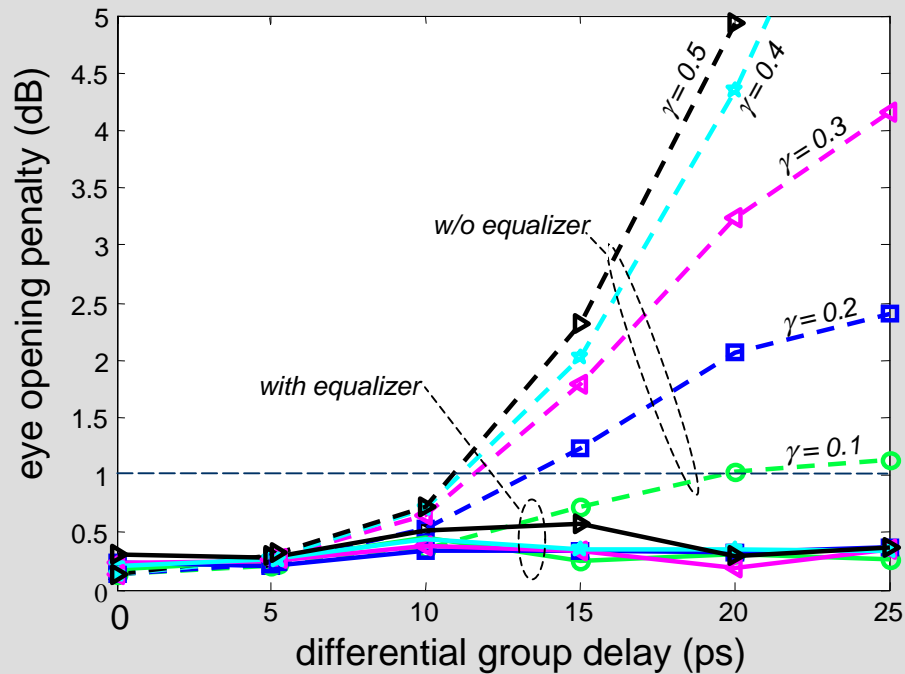
2b.)



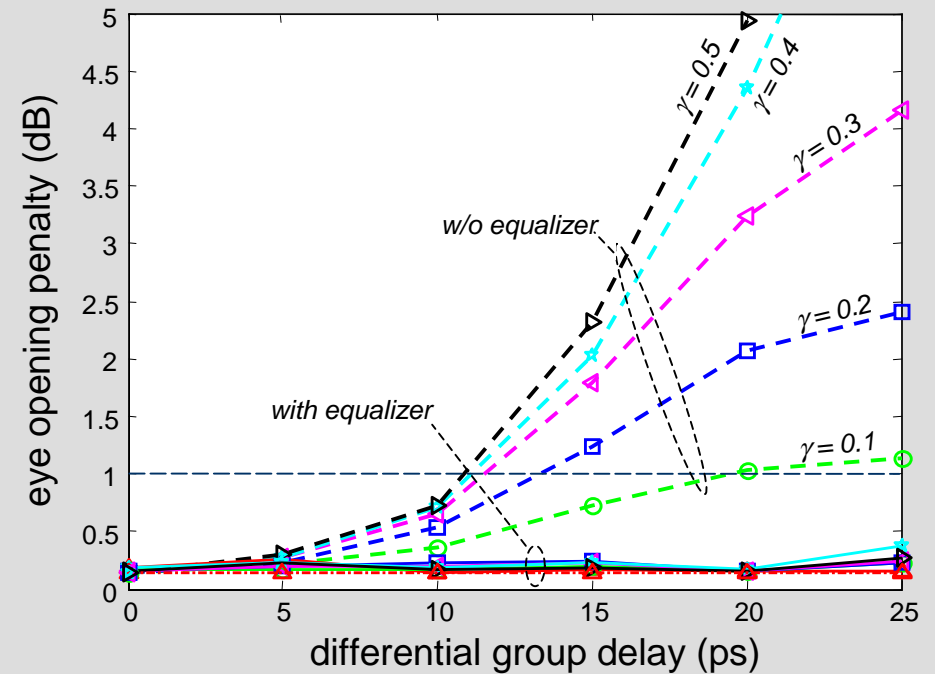
double filter setup

40Gb/s Results - PMD 1st order

single filter setup (filter order $n=2$)



double filter setup (filter order $n=2$)

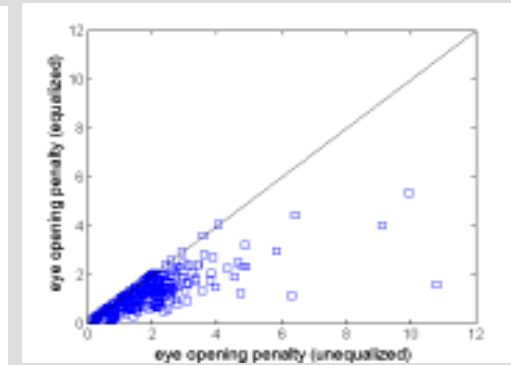
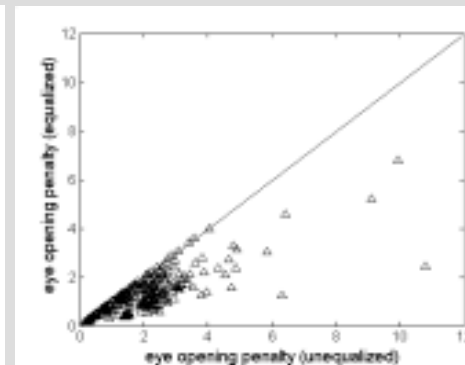
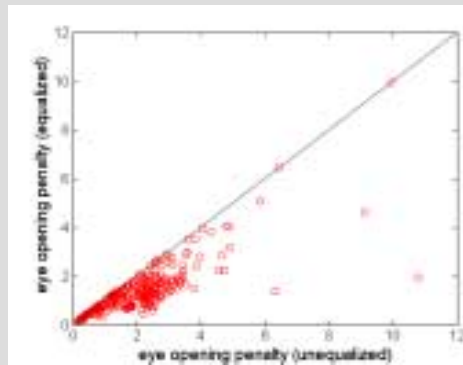


40Gb/s Results - PMD 1st and higher order

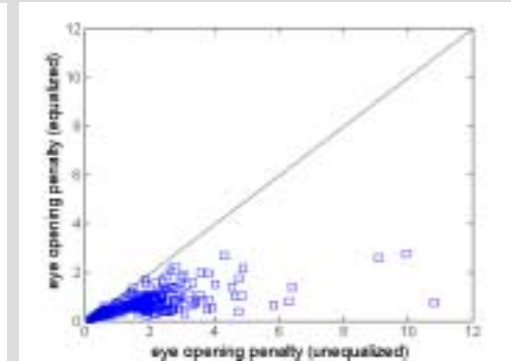
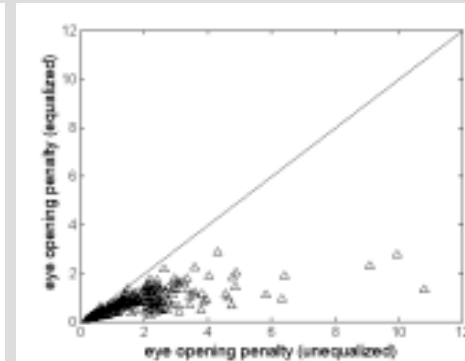
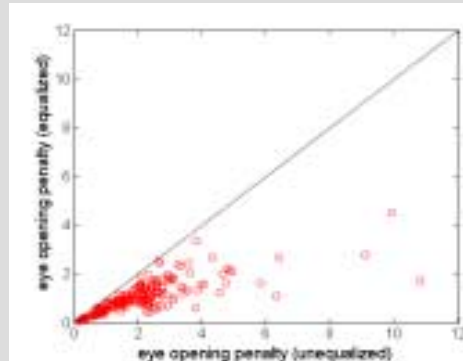
- simulated fiber span: $L=100\text{km}$, $D_{\text{PMD}}=1\text{ps}/\sqrt{\text{km}}$, $\text{PMD}_{\text{mean}}=10\text{ps}$

filter order $n=2$ $n=4$ $n=6$

single filter setup

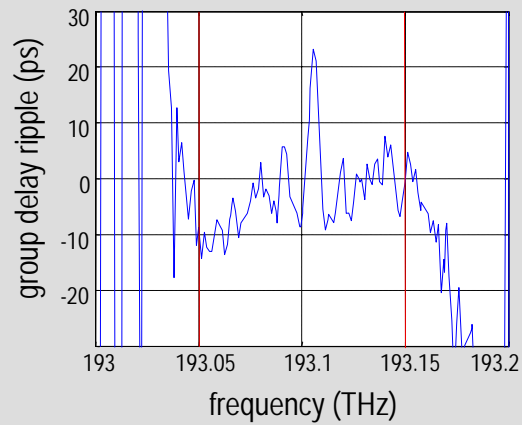


double filter setup



Group Delay Ripple Modeling

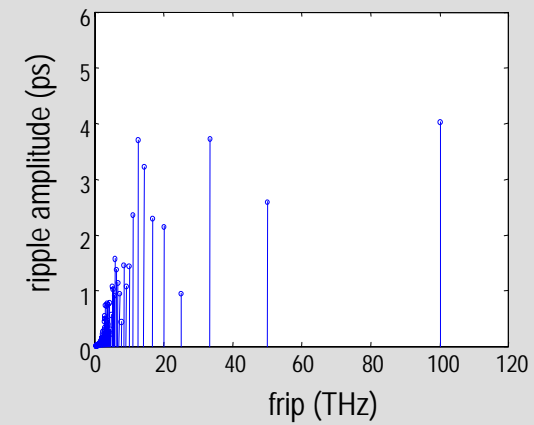
Group Delay Measurement



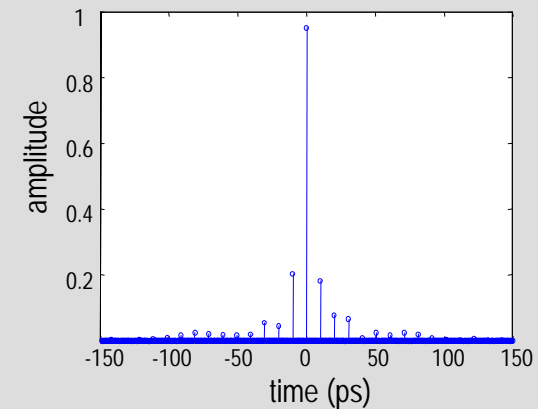
FFT



Ripple Spectrum



Impulse Response



$$t_{g,i}(\omega) = -\Delta t_{g,i} \cos \frac{\omega}{f_{rip,i}}$$

$$h_i(t) = \sum_{k=-\infty}^{\infty} J_k(\Delta t_{g,i} f_{rip,i}) e^{jk\phi_i} \delta_0(t + k / f_{rip,i})$$

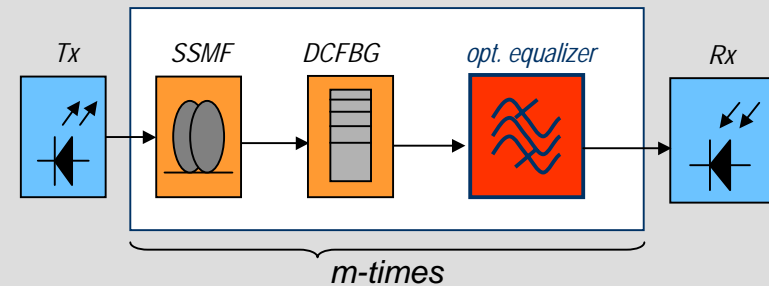
$$h(t) = h_1(t) * h_2(t) * \dots * h_I(t)$$

GDR Equalization Schemes

- equalization schemes

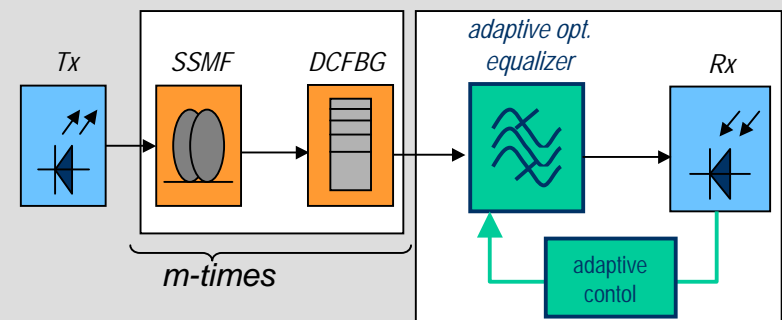
- optical inline compensation by modeling the inverse system

CFBG + Filter = Ripple Free Device



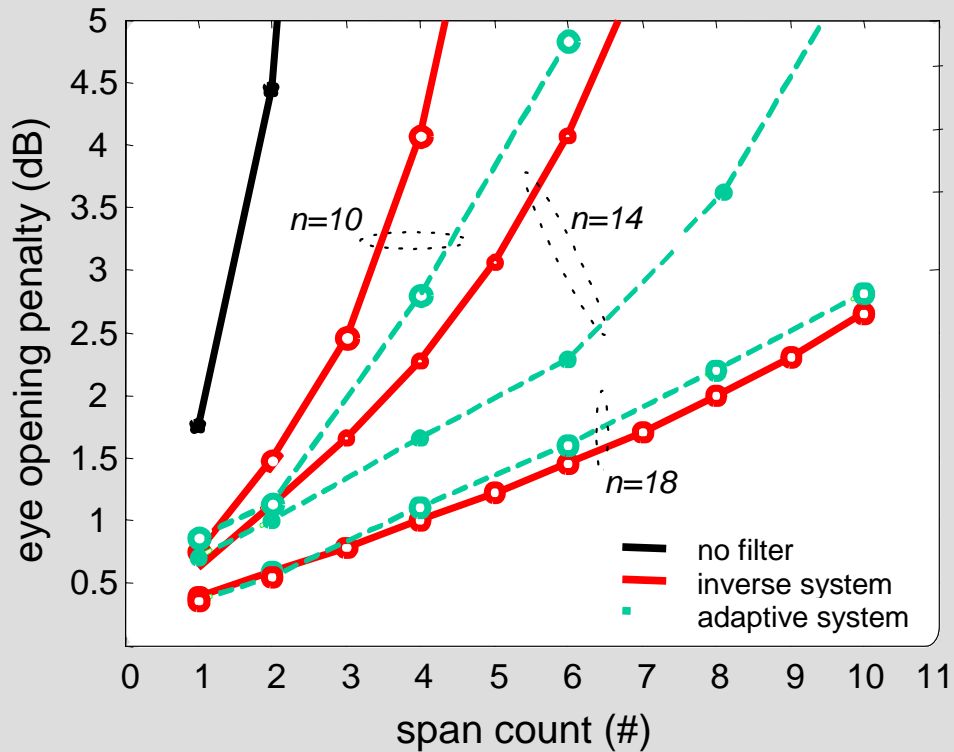
- post equalization with an adaptive optical filter

ripple mitigated tunable dispersion compensation with fixed DCFBGs

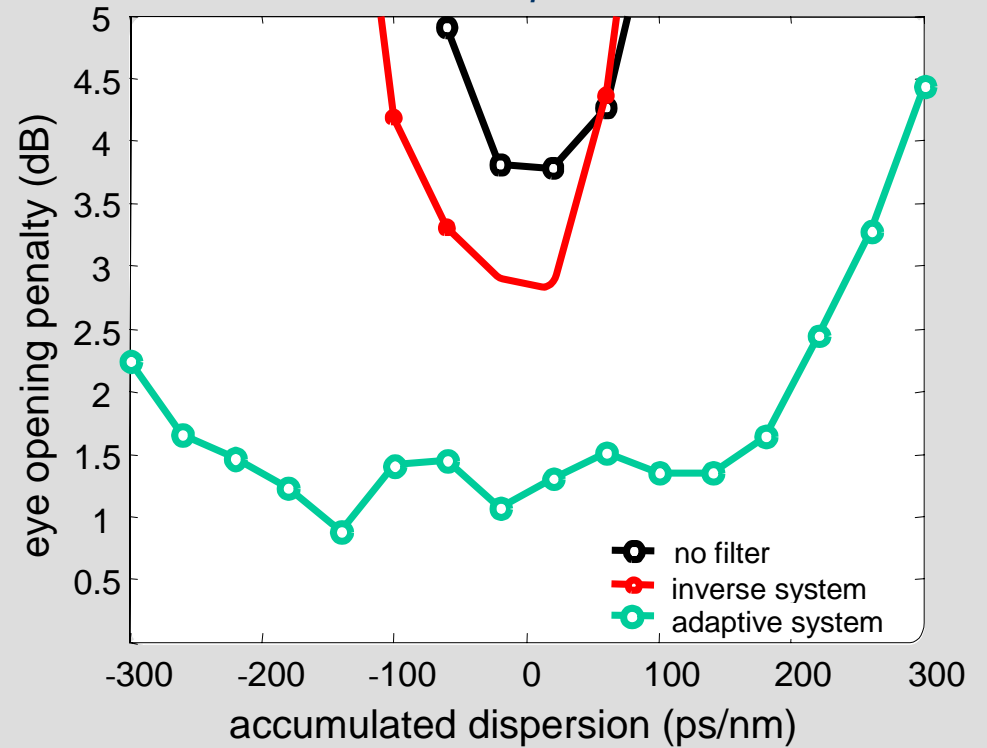


40Gb/s Results - Group Delay Ripple

equalization of group delay ripple only



equalization of group delay ripple @ 10dBm, 2spans, n=10





Summary

- **adaptive equalizer concept:**
 - excellent dispersion tolerance improvement for linear and nonlinear transmission
 - excellent SPM equalization
 - PMD equalization of 1st and higher order
 - group delay ripple compensation

**combined optical mitigation of
all single channel distortions**